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PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINES

by Albert F. Kascak Lewis Research Center Cleveland, Obio

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PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE

EFFECTS MACHINES

by Albert F. Kascak

Lewis Research Center

SUMMARY

This report presents some performance estimates of a high-speed peripheral-jet nuclear powered surface effects machine. Conclusions reached differ from previous studies in the literature because the new model uses a recently proposed nuclear air-plane reactor concept. This high-temperature reactor reduces shield weight and eliminates a heavy preheater previously required to obtain good thermodynamic efficiency. Payload fraction and reactor power are presented for various gross weights as a function of forward velocity and clearance height.

The parameters were varied over the following ranges: gross weight from 1000 to 5000 tons $(9.07\times10^5$ to 45.6×10^5 kg); forward velocity from 0 to 250 knots (0 to 129 m/sec); and obstacle clearing height from 10 to 50 feet (3.05 to 15.2 m). For these ranges, the payload varied from 0 to about 60 percent of the gross weight. The total reactor power varied from 400 to 10 000 megawatts. The study indicates that a 3000-ton $(27.2\times10^5$ -kg) nuclear surface effects machine could travel at speeds up to 250 knots (129 m/sec) at a 10-foot (3.05-m) clearance height, or as high as 50 feet (15.2 m) at reduced forward velocity.

In conclusion, a nuclear powered surface effects machine appears to be feasible for weights of 1000 to 5000 tons $(9.07\times10^5 \text{ to } 45.6\times10^5 \text{ kg})$ with payloads as high as 30 to 60 percent of the gross weight. Although reasonable performance potential has been shown by this study, some important problems have not been considered. Aerodynamic stability and maneuverability remain to be investigated.

INTRODUCTION

A nuclear surface effects machine is not a new concept. It was looked at in great detail in reference 1 where the authors used several General Electric Company 630-A gas

cooled reactors. Reference 1 concluded that the nuclear powered surface effects machines would have a small payload. It is the object of this study to update this analysis to include a nuclear airplane reactor concept that is proposed in reference 2. This analysis differs from reference 1 in that it uses this high-temperature reactor, thus reducing shielding weights and eliminating a need for a heavy preheater to obtain a good thermodynamic efficiency. This analysis uses a model of a high-speed peripheral-jet surface effects machine. The analysis includes a structural weight correlation given in reference 1, and a reactor-plus-shield weight correlation given in reference 2. The total power required (and therefore the powerplant weight) was determined by calculating the total vehicle drag and lift power.

Payload fraction and reactor power are calculated as a function of gross weight, forward velocity, and clearance height. These parameters were varied over the following ranges: gross weight from 1000 to 5000 tons $(9.07\times10^5 \text{ to } 45.6\times10^5 \text{ kg})$; forward velocity from 0 to 250 knots (0 to 129 m/sec); and an obstacle clearing height from 10 to 50 feet (3.05 to 15.2 m).

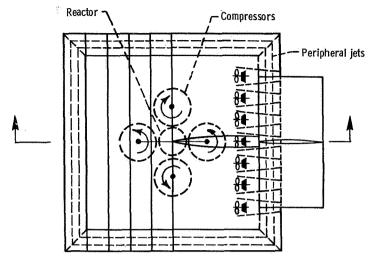
SYMBOLS

```
area. ft<sup>2</sup>: m<sup>2</sup>
Α
\mathbf{C}
              cushion length, ft; m
C^{D}
              drag coefficient, D/SCq<sub>A</sub>
              jet reaction coefficient
C_{T}
              lift coefficient, lift/SCq
C_{\mathbf{p}}
              specific heat at constant pressure
D
              drag, lb; kg
              cushion discharge coefficient, Q/CH \sqrt{2g\Delta P/\rho_A}
\mathbf{D}_{\mathbf{C}}
\overline{\mathbf{D}}_{\mathbf{C}}
               cushion discharge coefficient when X \rightarrow \infty
^{\mathrm{DP}}\mathrm{_{com}}
              pressure difference across compressor
              jet reaction force
F,
              Froude number, \sqrt{V_0^2/(gC)}
FR
               constant used in curve fit
FR<sub>12</sub>
               acceleration due to gravity
g
Η
              height of jet
```

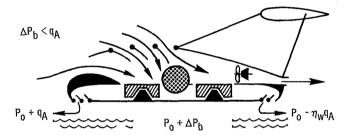
```
constant used in curve fit
\mathbf{m}
          ambient pressure, lb/ft<sup>2</sup>; N/m<sup>2</sup>
Po
          pressure in nozzle above ambient, 1b/ft^2; N/m^2
P_{t}
          air volume flow rate, ft<sup>3</sup>/sec; m<sup>3</sup>/sec
Q
          air dynamic head, \rho_{\rm A} {\rm V_o^2/(2g)},~{\rm lb/ft^2};~{\rm N/m^2}
\mathbf{q}_{\mathbf{A}}
S
           cushion beam, ft; m
t
          nozzle thickness, ft; m
Vo
           craft velocity, ft/sec; m/sec
\mathbf{v}_{\mathbf{T}}
          exit velocity of thrust jet
W
          weight, 1b; kg
          nondimensional jet thickness, (t/h)(1 + \sin \theta)
X
          pressure difference across jet, lb/ft<sup>2</sup>; N/m<sup>2</sup>
\Delta P
          base pressure, lb/ft<sup>2</sup>; N/m<sup>2</sup>
\Delta P_h
          temperature rise of jet, <sup>O</sup>F; K
\Delta T
           efficiency
η
           constant used in curve fit
\eta_{12}
           density of air
\rho_{\mathbf{A}}
           density of water
\rho_{\mathbf{W}}
 θ
          jet angle
Subscripts:
          front jet
1
2
           rear jet
3
           side jet
\mathbf{T}
           thrust jet
TH
           thermal
```

ANALYSIS

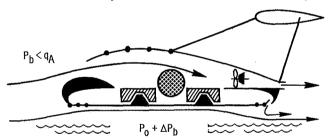
A conceptual layout of a nuclear powered surface effects machine is shown in figure 1. The plan view of the machine shows the machine as a square platform. The pressure below this platform, the base pressure, is above ambient. Thus, the pressure



(a) Plan view showing pheripheral jets, compressors, and reactor supplying power.



(b) Side view with velocity of craft less than cushion breakdown velocity.



(c) Side view with velocity of craft greater than cushion breakdown velocity.

Figure 1. - Conceptual design of nuclear powered surface effect machine.

difference between the bottom and the top of the platform results in a lift. To maintain the base pressure above ambient, a jet of air is directed downward below the platform and inward toward the center of the platform. This jet of air completely surrounds the periphery of the machine. Lift is produced by a pressure difference between the bottom and top surfaces of the platform rather than through the thrust produced by the peripheral jet. The air jet prevents the loss of the higher pressure base air from escaping to the outside.

An analysis of a stationary surface effects machine is given in reference 3. The object of the present analysis is to modify the stationary analysis of reference 3 to be appli-

cable to a moving, nuclear powered surface effects machine. The method by which this is done is shown in figure 1 (side view).

The surface effects machine operates in two distinct aerodynamic modes. The forward velocity of the craft can be either less than or greater than a critical velocity which is just enough to 'blow' the air cushion out from under the craft. This physical phenomenon is known as 'cushion breakdown.' It occurs when the dynamic pressure of the incoming air is approximately equal to the base pressure minus the ambient pressure. This study includes both regimes of operation.

The actual pressure distribution around the base of the craft is a function of the specific design of the craft; and therefore, is out of the scope of this report. A simplified model of the pressure distribution around the base of the craft was assumed which considered a constant, but different average pressure at the front, sides, and rear of the craft. The values of these average pressures were chosen so that they approximated the pressure distribution around a rectangular solid (which simulated the rectangular air cushion under the craft).

At velocities for which cushion breakdown does not occur, there are three distinct jets at the front, rear, and sides of the craft. Each of these jets must maintain a different pressure difference between the base platform region and the regions exterior to the craft. The region exterior to the front of the craft is assumed to be at ambient pressure plus the dynamic pressure. In other words, the incoming air is stagnated at the front of the craft. At the rear of the craft, a wake is produced; therefore, the region exterior to the rear of the craft is assumed to be at ambient pressure minus some fraction of the dynamic pressure. This fraction $\eta_{\rm W}$ is a complicated function of the geometry and the Reynolds number. In this analysis, $_{\rm W}$ was assumed to be 0.5, which is a representative value for flow around a flat plate. The region exterior to the sides of the craft was assumed to be at ambient pressure.

At velocities high enough to cause cushion breakdown, the front jet is turned off. The side jets are then used to "guide" the flow, and the rear jet is used to control the amount of flow under the craft. There is no total pressure difference between the base platform region and the region exterior to the front of the craft. Incoming air slows under the craft, increasing the static pressure to the required base pressure. The rear jet acts to produce a "blown nozzle," with the nozzle walls being formed by the rear jet and the ground. The nozzle constricts the flow, causing the flow to slow under the craft. The pressure exterior to the rear and to the sides of the craft is the same as in the operating mode existing before cushion breakdown, but at a higher dynamic pressure.

Figure 2 shows some of the fundamental parameters of a stationary surfaces effects machine. Reference 3 gives the following relations between these parameters:

$$X \equiv \frac{t}{H} (1 + \sin \theta) \tag{1}$$

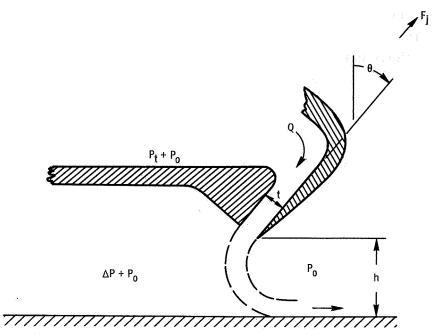


Figure 2. - Parameters of stationary annular jet surface effect machine.

$$\frac{\Delta P}{P_t} = 1 - e^{-2X} \tag{2}$$

$$Q = D_{C}CH\sqrt{\frac{2g\Delta P}{\rho_{A}}}$$
(3a)

where

$$D_{C} = \overline{D}_{C} \tanh \sqrt{\frac{X}{2[\overline{D}_{C}(1 + \sin \theta)]^{2}}}$$
 (3b)

and

$$\overline{D}_{C} = \lim_{X \to \infty} D_{C} = \frac{1}{2} \left[1 + \frac{\cos \theta}{\frac{\pi + 2}{\pi - 2} (1 + \sin \theta) - \sin \theta \cos \theta} \right]$$
(3c)

$$\mathbf{F_{j}} = \mathbf{C_{j}}\mathbf{Ct} \ \Delta \mathbf{P} \tag{4a}$$

where

$$C_{j} = \frac{1}{1 - e^{-2X}} + \frac{1}{2X}$$
 (4b)

Applying these stationary results (eqs. (1) to (4)) to the dynamic model leads to the following sets of equations. Consider the front jet (subscript 1) operating at speeds below cushion breakdown:

$$t_1 = \frac{X_1 H}{1 + \sin \theta_1} \tag{5a}$$

$$\Delta P_1 = \Delta P_b - q_A \tag{5b}$$

$$P_{t1} = \frac{\Delta P_1}{\left(1 - e^{-2X_1}\right)} + q_A \tag{5c}$$

$$Q_1 = D_C(X_1)SH\sqrt{\frac{2g \Delta P_1}{\rho_A}}$$
 (5d)

$$\mathbf{F}_{\mathbf{j}\mathbf{1}} = \mathbf{C}_{\mathbf{j}}(\mathbf{X}_{\mathbf{1}})\mathbf{S}\mathbf{t}_{\mathbf{1}} \Delta \mathbf{P}_{\mathbf{1}} \tag{5e}$$

For speeds above cushion breakdown, the front jet is turned off:

$$t_1 = 0 (6a)$$

$$\Delta P_1 = 0 \tag{6b}$$

$$P_{t,1}$$
 = Not defined (6c)

$$Q_1 = 0 (6d)$$

$$\mathbf{F}_{\mathbf{j}\mathbf{1}} = \mathbf{0} \tag{6e}$$

Consider the rear jet (subscript 2) operating at speeds below cushion breakdown:

$$t_2 = \frac{X_2 H}{1 + \sin \theta_2} \tag{7a}$$

$$\Delta P_2 = \Delta P_b + \eta_W q_A \tag{7b}$$

$$P_{t2} = \frac{\Delta P_2}{\left(1 - e^{-2X_2}\right)} - \eta_W q_A \tag{7c}$$

$$Q_2 = D_C(X_2)SH \sqrt{\frac{2g \Delta P_2}{\rho_A}}$$
 (7d)

$$\mathbf{F}_{12} = \mathbf{C}_{1}(\mathbf{X}_{2})\mathbf{St}_{2} \Delta \mathbf{P}_{2} \tag{7e}$$

For speeds above cushion breakdown, the rear jet acts as the top surface of a blown nozzle. The height of the rear jet is less than the clearance height of the craft and can be calculated from Bernoulli's Law:

$$H_2 = \left[1 - \sqrt{\frac{q_A - \Delta P_b}{(1 + \eta_W)q_A}}\right] H$$

If H₂ is substituted in place of H, the preceding equations describe the condition after cushion breakdown.

The side jets (subscript 3) can be considered the same as in the stationary analysis of reference 3. Therefore, they are described by equations (1) to (4).

To propel the craft forward, a thrust jet (subscript T) is included in the configuration shown in figure 1. The analysis of this jet follows directly from mass and momentum conservation:

$$V_{T} = \frac{V_{O}}{2} \left(1 + \sqrt{1 + \frac{2D}{A_{T}q_{A}}} \right)$$
 (8a)

$$Q_{T} = A_{T}V_{T}$$
 (8b)

$$P_{tT} = \frac{\rho_A V_T^2}{2g}$$
 (8c)

To drive these four jets (front, rear, side, and thrust), incoming air is compressed to a value above the jet total pressure. It is assumed that a fraction of the incoming dynamic pressure $\eta_{\rm ram} {}^{\rm q}_{\rm A}$ can be converted to ram pressure, and if a duct loss is assumed to be some fraction of the jet total pressure, the compressor pressure difference is

$$DP_{com} = \frac{P_{T}}{\eta_{duct}} - \eta_{ram} q_{A}$$
 (9)

The power necessary to drive the compressor is

$$Power = \frac{Q \times DP_{com}}{\eta_{com}}$$
 (10)

when $\eta_{\rm com}$ is the efficiency of the compressor. If the engine that is driving this compressor has a thermal efficiency of $\eta_{\rm TH}$, then the rate of heat transferred to the jet is

$$q_{j} = \frac{(1 - \eta_{TH})Power}{\eta_{TH}}$$
 (11)

and the temperature rise of the air jet is $\Delta T = q_j/C_p \rho_A Q$. The total reactor power is the sum of the individual powers divided by the thermal efficiency:

Reactor power =
$$\frac{Power_1 + Power_2 + Power_3 + Power_T}{\eta_{TH}}$$
 (12)

The forces on the craft can be categorized in two classics - those producing lift and those producing drag. The lift forces on the craft are as follows: aerodynamic lift; the jet reaction force from the front, rear, and side jets; and the lift due to the increased base pressure. These lift forces must be equal to the gross weight of the craft:

$$W_{G} = St_{1} \cos \theta_{1}(C_{j1} - 1)DP_{1} + St_{2} \cos \theta_{2}(C_{j2} - 1)DP_{2} + 2Ct_{3} \cos \theta_{3}(C_{j3} - 1)DP_{3}$$

$$+ (\Delta P_{b} + C_{T}q_{A})SC \qquad (13)$$

For a given aspect ratio, equation (13) can be solved for the length of the craft.

There are four drag forces on the craft: aerodynamic drag, jet reaction drag from an unbalance of the front and rear jet reaction forces, wave drag, and a momentum drag. The aerodynamic drag is given by

$$D_{aero} = C_{D}SCq_{A}$$
 (14a)

The jet drag is given by

$$D_{jet} = St_2 \sin \theta_2 C_{j2} DP_2 - St_1 \sin \theta_1 C_{j1} DP_1$$
 (14b)

Reference 4 gives a method for calculating the wave drag of a rectangular craft moving over water in terms of the Froude Number:

$$\mathbf{Fr} = \sqrt{\frac{v_o^2}{gC}}$$

$$D_{\text{wave 4}} \eta_{12} \left(\frac{\text{Fr}}{\text{Fr}_{12}} \right)^{m} \left(\frac{4\Delta P_{b}^{2} \text{S}}{\rho_{W}} \right)$$
 (14c)

For an aspect ratio of 1, the following curve-fitting constants gave the best results.

$$\eta_{12} = 0.815$$

$$\mathbf{Fr}_{12} = 0.59$$

For $Fr < Fr_{12}$,

$$m = 1.45$$

and for $Fr > Fr_{12}$,

$$m = -1.82$$

The momentum drag is the result of stagnating air under the craft and is given by

$$D_{\text{mom}} = \frac{\rho_{A}}{g} (Q_{1} + Q_{2} + Q_{3}) V_{0}$$
 (14d)

The payload is the weight of the disposable load, that is, the gross weight minus the weight of the structure, the weight of the powerplant, and the weight of the reactor shield. The weight of the structure was given in reference 1 as

$$W_{struct} = 2.36 W_{gross} \Delta P_b^{-0.481}$$
 (15a)

The weight of the powerplant was assumed to be 2 pounds per shaft horsepower (1.22 g/W). The weight of the shield was given in reference 2 as

$$W_{\text{shield}} = 220\ 000\ (\text{lb})\ \sqrt{\frac{\text{Total reactor power (MW)}}{300\ (\text{MW})}}$$

$$W_{\text{shield}} = 0.066 \times 10^4 \text{ (kg)} \sqrt{\frac{\text{Total reactor power (MW)}}{300 \text{ (MW)}}}$$

These equations along with the following assumed quantities allow solution for the payload and total reactor power as a function of forward velocity, obstacle clearing height, and gross weight:

Thermal efficiency	. 20
Compressor efficiency), 85
Ram recovery efficiency). 90
Duct efficiency). 90
Lift coefficient). 01
Drag coefficient). 01
Aspect ratio	. 00
Thrust area to platform area ratio	0.03

RESULTS AND DISCUSSION

The objective of this study was to determine the payload fraction and the reactor power required to fly a specified gross weight surface effects machine over a given height obstacle at a given forward velocity. The parameters were varied over the following ranges: gross weight from 1000 to 5000 tons (9.07×10⁵ to 45.6×10⁵ kg); forward velocity from 0 to 250 knots (0 to 129 m/sec); and an obstacle clearing height from 10 to 50 feet (3.05 to 15.2 m).

Besides these three primary parameters, there are three secondary variables in the

analysis: jet angle, jet thickness, and base pressure. Before the three primary variables can be examined in detail, these secondary parameters must be fixed in some manner. Reference 3 showed that as the jet angle was increased from 0° to 90° , the hover power continually decreased; but at the same time jet mixing increased. The theory of reference 3 is not valid for large amounts of jet mixing; therefore, a compromise jet angle of 60° was chosen for this study.

Reference 3 showed that a nondimensional jet thickness X equal to 0.7 minimized the hover power, as the result of a compromise between the increased pressure necessary to maintain the jet and the jet reduction of the discharge coefficient. In the dynamic case, two other factors must be considered: the momentum drag and jet drag. Figure 3 shows the optimum nondimensional jet thickness for the front, rear, and side jets against velocity of the craft for a typical thrust efficiency of 0.5. It can be seen that the front nozzle requires a very large jet thickness. The front nozzle thickness was arbitrarily limited to X equal to 0.7. The rear and side nozzle thickness generally decreased with increasing velocity.

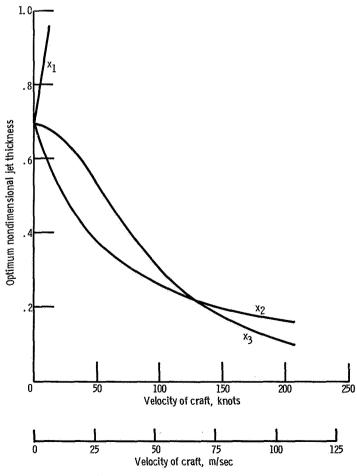


Figure 3. - Optimum nondimensional jet thickness. Thrust efficiency, 0.5.

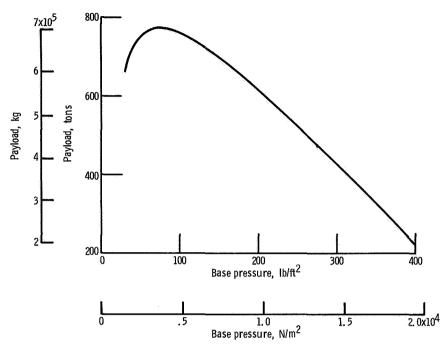


Figure 4. – Payload as function of base pressure. Gross weight, 1500 tons $(13.6 \times 10^5 \text{ kg})$; velocity of craft, 0; clearance height, 10 feet (3.05 m).

The last of the secondary parameters is the cushion base pressure. Figure 4 shows the payload against base pressure for a typical nuclear powered surface effects machine. It can be seen that the payload has a maximum at about 75 pounds per square foot (3.585 $\times 10^3$ N/m²). This is the result of a compromise between structural weight and power-plant weight. For the rest of the calculations, the base pressure was assumed to be 75 pounds per square foot (3.585×10³ N/m²).

With the secondary parameters specified, the three primary variables can be examined in detail. This was done in the calculations by varying one parameter and holding the other two parameters constant. The numerical value of the parameters held fixed was chosen so as to represent typical results.

Figure 5 shows the variation of the payload and total reactor power against obstacle clearing height for a gross weight of 3000 tons $(27.2\times10^5 \text{ kg})$ and a forward velocity of 50 knots (129 m/sec). Figure 5(a) shows that as the height increases from 10 to 50 feet (3.05 to 15.2 m), the payload drops from about 60 to about 10 percent of the gross weight. Figure 5(b) shows that as the height increases from 10 to 50 feet (3.05 to 15.2 m), the total reactor power increases from about 1000 to about 5000 megawatts.

Figure 6 shows the variation of the payload and total reactor power against forward velocity for gross weight of 3000 tons $(27.2\times10^5 \text{ kg})$ and an obstacle clearing height of 10 feet (3.05 m). Figure 6(a) shows that as the velocity increases from 0 to 250 knots (0 to 129 m/sec), the payload decreases from 60 to 30 percent of the gross weight. At

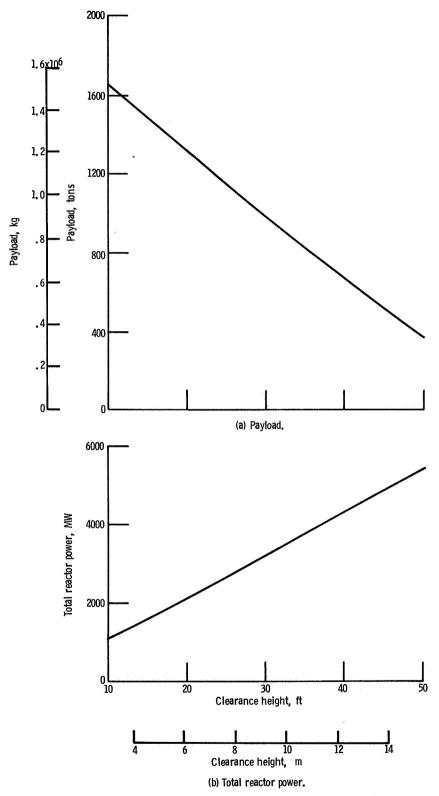


Figure 5. - Payload and total reactor power as function of clearance height. Gross weight, 3000 tons (27, 2x10⁵ kg); velocity of craft, 50 knots (25, 7 m/sec).

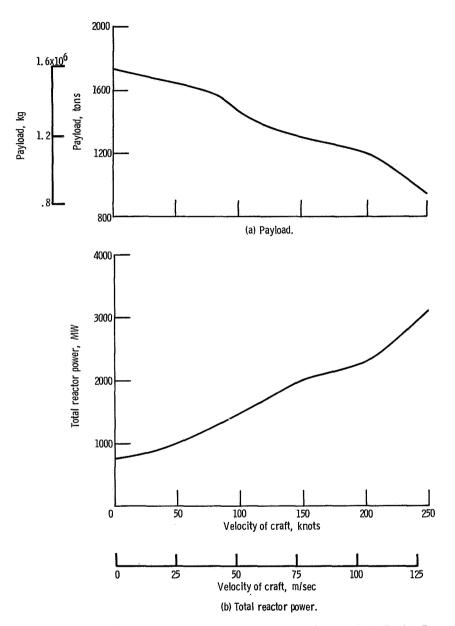


Figure 6. - Payload and total reactor power as function of velocity of craft. Gross weight, 3000 tons (27. $2\times10^{+5}$ kg); clearance height, 10 feet (3.05 m).

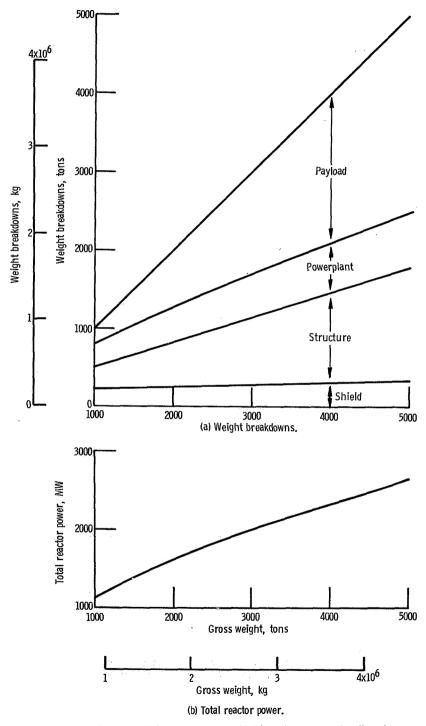


Figure 7. - Weight breakdowns and total reactor power as function of gross weight. Clearance height, 10 feet (3.05 m); velocity of craft, 150 knots (77.2 m/sec).

150 knots (77.2 m/sec) the payload is about 45 percent of the gross weight. Figure 6(b) shows that as the velocity increases from 0 to 250 knots (0 to 129 m/sec), the total reactor power increases from about 750 to 3000 megawatts. The sharpest increase takes place above 200 knots (103 m/sec). At 150 knots (77.2 m/sec) the power is about 2000

Figure 7 shows the variations weight breakdowns and total reactor power against gross weight for a forward velocity of 150 knots (77.2 m/sec) and an obstacle clearing height of 10 feet (3.05 m). Figure 7(a) shows that as the gross weight increases from 1000 to 5000 tons (9.07×10 5 to 45.6×10 5 kg), the payload increases from 20 to about 50 percent of the gross weight. At a gross weight of 3000 tons (27.2×10 5 kg), the reactor shield weighed 285 tons (2.56×10 5 kg), the structure weighed 875 tons (7.94×10 5 kg), the powerplant weighed 540 tons (4.90×10 5 kg), and the remaining payload was 1310 tons (11.9×10 5 kg). Figure 7(b) shows that as the gross weight increased from 1000 to 5000 tons (90.7×10 5 to 45.6×10 5 kg), the total reactor power increased from about 1100 to 2600 megawatts. At a gross weight of 3000 tons (27.2×10 5 kg), the total reactor power was about 2000 megawatts.

Many variables were calculated besides the ones discussed. Table I (p. 19) gives the detailed results of the calculations. This table presents the various pressures, flow rates, shaft horsepowers, drags, etc. For the range of parameters given, the payload varied from 0 to about 60 percent of the gross weight and the total reactor power varied from 400 to about 10 000 megawatts.

CONCLUSIONS

The objective of this study was to present some performance characteristics of a high velocity, nuclear powered surface effects machine. Payload fraction and reactor power were calculated as a function of gross weight, forward velocity, and clearance height. These parameters were varied over the following ranges: gross weight from 1000 to 5000 tons $(9.07\times10^5 \text{ to } 45.6\times10^5 \text{ kg})$; forward velocity from 0 to 250 knots (0 to 129 m/sec); and an obstacle clearing height from 10 to 50 feet (3.05 to 15.2 m).

For the range of parameters given, the payload varied from 0 to about 60 percent of the gross weight. The total reactor power varied from 400 to 10 000 megawatts. A 3000-ton $(27.2\times10^5$ -kg) nuclear surface effects machine could travel at speeds up to 250 knots (129 m/sec) at a 10-foot (3.05-m) clearance height, or as high as a 50-foot (15.2-m) clearance height at a reduced velocity.

A nuclear powered surface effects machine appears feasible for gross weights between 1000 and 5000 tons $(9.07\times10^5 \text{ and } 45.6\times10^5 \text{ kg})$. Payloads as high as 30 to 60 percent of the gross weight appear possible. Vehicle forward velocities up to 250 knots

(129 m/sec), and obstacle clearing heights of 50 feet (15.2 m) do not require excessive reactor powers. In short, the indicated performance characteristics are attractive. Obviously, some important problems remain to be investigated such as aerodynamic stability and vehicle maneuverability.

Lewis Research Center,

National Aeronautics and Space Administration, Cleveland, Ohio, July 7, 1969, 122-28.

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TABLE I. - PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

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1000.	159 159 75 239 239 188	133 235 235 8	Ħ	
50° 1000° 10° 10° 10° 10° 10° 10° 10° 10°		24 5 5 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7	1 1	2229
1000.	159 1599 113, 13, 13, 13, 13, 13, 13, 13, 13, 13	29200 29200 29200 58400 117000 435,	23400 23400 23400 23400 1910000 123000	24600 49300 599 119 111 111 110 110 110 110 110 110 1
VELOCITY, KNDTS GROSS WEIGHT, TONS CLEARANCE HEIGHT, FT	I ENGTH, FT WIDTH, FT BASE PRESSURE, LB/FT*FT WEIGHT OF PAYLDAD, TONS WEIGHT OF POWER PLANT, TONS WEIGHT OF REACTOR SHIELD, TONS	REAR COMPRESSOR S.H.P. SIDE COMPRESSOR S.H.P. SIDE COMPRESSOR S.H.P. THRUST COMPRESSOR S.H.P. TOTAL S.H.P. AFRO DYNAMIC DRAG. LB	JET DRAG, L9 MOMENTUM DRAG, LB AGRO DYNAMIC LIFT, LB REAR JET LIFT, LB SIDE JET LIFT, LB STOR JET LIFT, LB STOR JET LIFT, LB STOR JET LIFT, LB REAR JET LIFT, LB REAR JET LIFT, LB REAR COMPRESSOR AIR FLOW, FT**3/SEC	KERK CUMMRESSON AIR FLOW, FIRE3/SEC THRUST COMPRESSON AIR FLOW, FIRE3/SEC THRUST COMPRESSON AIR FLOW, FIRE3/SEC TOTAL AIR FLOW, FIRE3/SEC FROMT JET AREA, FIRET REAR JET AREA, FIRET TOTAL AREA, EIRET THRUST COMPRESSON PRESSURE DIFFERENCE, LB/FIRET THRUST COMPRESSON PRESSURE, LB/FIRET FROMT NOTZLE PRESSURE, LB/FIRET THRUST NOTZLE PRESSURE, LB/FIRET THRUST NOTZLE PRESSURE, LB/FIRET THRUST NOTZLE PRESSURE, BTU TOTAL JET HEAT TRANSFER, BTU

TABLE I. - Continued. PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

GRDSS WFIGHT, TONS CLEARANCE HEIGHT, FT	20.	.000 20.	•000 50•	20.	20.	20.
	156.	155.	155.	155	155.	154.
MIDIH. FI RASE ORESSURE. LB/FT*FT	75.	75.	75.	75.	75.	75.
WEIGHT OF PAYLUAD, TONS	304.	273.	. 529.	176.	103.	4.
OF POWER PLANT, TON	228.	251.	283.	322.	378.	250
WEIGHT OF REACTOR SHIFLD, JUNS	185	282	281.	281.	281.	280.
	57000	55700	52300	46700.	39400	30600
REAR COMPRESSOR S.P.D.	57000.	59600	62200	65600.	70100.	75900.
	114000.	113000.	112000.	111000.	112000.	114000.
THRUST COMPRESSOR S.H.P.	•0	22300.	56800.	99100	156000.	226000.
TOTAL S.H.P.	228000.	251000.	283000	322000.	378000	447000
TAL REACTOR POWER, MEG-W	820	400%	0007	1200.	4240	6650
AERO DYNAMIC DRAG. LB	• •	28100	22406	10700	6320.	4200
	-323.	-18500.	-13700.	-765.	19100.	45700.
MOMENTUM DRAG. LB	0	64400	120000.	166000.	204000	233000
TOTAL DRAG. LB	-323.	74200.	130000.	1 79000.	234000	290000
AFRO DYNAMIC LIFT. LB	0	269.	1070		4260.	.0699
FRONT JET LIFT, LB	45600.	44800	42 700°	59300	54500	66200
XTAX JT - 1.5	91400	97000	98100	102000	106000	109000
CHAID LIFT I B	1820000	1810000.	1800000	1800000	1790000	1790000.
FRONT COMPRESSOR AIR FLOW, FT**3/SEC	41000		233000.	223000.	209000	190000
LOW. FT**3/SEC	240000	185000.	1 70 00 0.	160000.	152000.	147000.
DE COMPRESSOR ATR FLOW. FT**3/SEC	481000.	454000	414000.		334000	299000
THRUST COMPRESSOR AIR FLOW, FT**3/SEC	0 000	160030	220000	.00000	311 000.	9000700
TOTAL A TO FLOW, FIRM 3/SEC	.000796	1170	1160	1160	1160.	1160.
JET AREA. F	1160.	668	547	467.	405	358
SIDE JET ARFA. FT*FT	2320	20.60	1700.	1370.	1 090	875.
THPUST JET AREA, FT*FT		724.	721.	719.	717.	716.
TOTAL AREA, FT*FT	24200.	24100.	24000	24000	23900	23900
,	0	1.00	4 0	10.	* 00°	28.
COMPRESSOR PRESSORE DIFFERENCE.	• T T T	. 601	103.	102	215	241
REAR (N)MORENOUS PRENOURN DIFFERENCE LENTER:	• ; • : : : : : : : : : : : : : : : : : : :	116.	126.	139.	157.	178.
ن •	• • •	65.	121.	174.	236.	300.
-	• 66	•66	.86	9.6	• 46	•06
AR NOZZLE PRESSURF, LB/FT*FT	100.	136.	158.	181.	208.	239.
SINE NOZZLE PRESSURF. 18/FT*FT	100.	106.	117.	133.	155.	183.
THRUST NOZZLE PRESSURE, LB/FT*FT	o	26	112.	165.	226.	293.
FRONT JET HEAT TRANSFER, BTU	161000.	158000.	148000.	132000.	111000.	86400*
	161000.	169000.	176000.	185000.	198000.	222000
SIDE JET HEAT TRANSFER, BIU	327000	320000	319000	280000	210000	640000
THREST OFF THAT TRANSFER BILL	645000	100000	800000	912000.	1070000	1260000.
FRONT LET TEMPERATURE RISE. DEG. F	36	35.	34.	32.		24.
FMPFRATURE RISE + DEG. F	36.	• 64	55.	.29	. 07	78.
SIDE JET TEMPERATURE RISE. DEG. F	36.	38.	41.	45.	51.	58.
THPUST JET TEMPERATURE RISE. DEG. F	0	21.	3.6	56.	76.	97.
t cité du la cité de la constitue de la consti						

250. 2000. 10.	224. 224. 75. 480. 637.	574. 0. 42500. 97500.	637000. 2370. 108000. 1330. 70000.	165000. 344000. 108000. 34600. 86600.	3760000. 0. 44200. 118000. 879000.	63. 186. 1500. 50200. 215.	264. 264. 215. 578. 412.	120000. 276000. 1400000. 1800000. 00. 145. 125. 86.
200. 2000. 10.	225. 225. 75. 669. 483. 270.	578. 0. 40400. 86600. 356000.	483000. 1800. 69900. 2020. 73800.	mi co	3810000. 0. 55200. 144000. 768000.	0. 95. 279. 1520. 50800. 138.	247. 280. 2138. 138. 364. 307.	114600. 245000. 1010000. 1370000. 0. 1111. 710. 76.
150. 2000. 10.	226. 226. 75. 730. 435. 256.	579. 0. 58200. 80700. 296000.	435000. 1620. 39500. 3430. 113000.	171000. 326000. 39500. 53400. 83200.	3820000. 0. 100000. 179000. 688000. 966000.	207. 426. 1530. 51000. 77.	272. 201. 202. 77. 307. 253. 264.	165000. 228000. 838000. 1230000. 68. 68. 68.
100. 2000. 10.	226. 226. 75. 328.	580. 18500. 53800. 78000.	328000. 1220. 17600. 7180. 48600.	193000. 266000. 17600. 17900. 49600.	3840000. 129000. 117000. 228000. 560000.	848. 295. 693. 1530. 51100. 34.	216. 160. 148. 88. 222. 172. 172.	152000. 221000. 502000. 927000. 70. 70. 68.
50. 2000. 10.	227. 227. 75. 1020. 220.	581. 35200. 45500. 79800. 60000.	220000. 822. 4420. 25400.	120000. 149000. 4420. 29400. 41000.	3850000. 165000. 127000. 296000. 380000.	850. 408. 1190. 1540. 51400.	168. 126. 74. 97. 158. 120.	129000. 226000. 170000. 623000. 54. 41. 24.
2000.	227. 227. 75. 1090. 166.	582. 41600. 41600. 83200.	166000. 620. 0. 0.	-235 -235 -235 -0 -33300 -66600	3870000. 176000. 175000. 350000. 701000.	852. 847. 1690. 1550. 51600.	1111- 1111- 990- 1000- 1000-	118000 235000 470000 36 36 36 36
VELOCITY, KNOTS GROSS WFIGHT, TONS CLEARANCE HEIGHT, FT	LENGTH, FT WIOTH, FT BASE PRESSURE, LB/FT*FT WFIGHT OF PAYLJAD, TONS WFIGHT OF PAMER PLANTS SHIFLD. TONS		TOTAL S.H.P. TOTAL REACTOR POWER, MEG-W AFRO DYNAMIC DRAG. LB HET DAG. LB	MOMENTUM DRAG. LB TOTAL DRAG. LB AFRO DYNAMIC LIFT. LB FRAMT JET LIFT. LB PRAM JET LIFT. LB SIDE JET LIFT. LB	CUSHION LIFT, LB FRONT COMPRESSOR AIR FLOW, FT**3/SFC RFAR COMPRESSOR AIR FLOW, FT**3/SFC SIDE COMPRESSOR AIR FLOW, FT**3/SFC THRUST COMPRESSOR AIR FLOW, FT**3/SEC TOTAL AIP FLOW, FT**3/SEC	ш	BEAR CTMPRESSOR PRESSURE DIFFERENCE, LB/FT*FT SIDE COMPRESSOR PRESSURE DIFFERENCE, LB/FT*FT THRUST COMPRESSOR PRESSURE DIFFERENCE, LB/FT*FT FRONT NO7ZLE PRESSURE, LB/FT*FT RFAR NO7ZLE PRESSURE, LB/FT*FT SIDE NO7ZLE PRESSURE, LB/FT*FT THRUST NO7ZLE PRESSURE, LB/FT*FT THRUST NO7ZLE PRESSURE, LB/FT*FT	FRANCIS JET HEAT TRANSFER, STO SIDE JET HEAT TRANSFER, BTU THRUST JET HEAT TRANSFER, BTU TOTAL JET HEAT TRANSFER, BTU FOOT JET TEMPERATURE RISE, DEG. F BEAR JET TEMPERATURE RISE, DEG. F SIDE JET TEMPERATURE RISE, DEG. F THRUST JET TEMPERATURE RISE, DEG. F AVERAGE AIR TEMPERATURE RISE, DEG. F

TABLE I, - Continued. PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

184. 230. 2000. 2000. 20. 20.		82 1010 1010 89 89 319 548 89 68 68 68 68 68 68 68 72 89 170 92 92 92 92 92 92 92 92 92 92 92 92 92	275. 352. 329. 373. 116. 182. 399. 521. 342. 464. 390. 0. 24300. 232000. 49000. 209000. 167000. 209000. 241000. 2850000. 110. 134.
138. 2000. 20.	221. 221. 75. 128. 930. 374. 568.	135000. 619000. 619000. 32100. 32100. 384000. 384000. 32100. 117000. 117000. 122000. 346000. 150000. 1600. 1600. 1600. 1600. 1600. 1600. 1600. 1600.	229. 354. 18. 317. 259. 20500. 381000. 1750000. 2630000. 2631000.
92. 2000. 20.	222. 222. 75. 75. 629. 308. 569.	107000. 159000. 2350. 2350. 14300. 348000. 348000. 348000. 14300. 3690000. 269000. 269000. 269000. 269000. 274.	169. 231. 90. 230. 176. 12000. 30200. 451000. 906000. 1780000. 55.
46. 2000. 20.	223. 223. 75. 747. 428. 254. 571.	90500 159000 4280000 4280000 28600 28600 23600 23600 34000 3710000 3710000 371000 444000 159000 1690 1690 175	129. 113. 97. 164. 201000. 256000. 449000. 305000. 1210000.
2000. 2000.	223. 223. 75. 879. 327. 222. 573. 81800.	81800. 164000. 327000. 1220. 1220463. 065400. 65500. 3740000. 3740000. 345000. 689000. 1380000. 1500.	111. 0. 99. 100. 231000. 231000. 462000. 925000. 36. 36.
VELOCITY, KVOTS GROSS WEIGHT, TONS CLEARANCE HEIGHT, FT	LENGTH, FT WIDTH, FT RASE PRESSURE, LB/FT*FT RASE PRESSURE, LB/FT*FT WEIGHT OF PAYLOAD, TONS WEIGHT OF REACTOR SHELD, TONS WEIGHT OF REACTOR SHELD, TONS WEIGHT OF STRUCTURE, TONS FRONT COMPRESSOR, S.H.P.	6-W 6-W 100. FT**3/SEC 100. FT**3/SEC 100. FT**3/SEC 100. FT**3/SEC 100. FT**3/SEC 100. FT**3/SEC 100. FT**3/SEC	SIDE COMPRESSOR PRESSURE DIFFERENCE, LB/FT*FT THRUST COMPRESSOR PRESSURE DIFFERENCE, LB/FT*FT FRONT NOZZLE PRESSURE, LB/FT*FT STDE NOZZLE PRESSURE, LB/FT*FT THRUST NOZZLE PRESSURE, LB/FT*FT FRONT JET HEAT TRANSFER, BTU STOR JET HEAT TRANSFER, BTU THRUST JET HEAT TRANSFER, BTU THRUST JET HEAT TRANSFER, BTU TOTAL JET TEMPERATURE RISE, DEG, F RANT JET TEMPERATURE RISE, DEG, F THRUST JET TEMPERATURE RISE, DEG, F THRUST JET TEMPERATURE RISE, DEG, F

100. 2000. 30.	218. 218. 75. 0. 1040. 396. 559.	53400. 170000. 245000. 576000. 1040000. 16300. 134000.	518000. 15800. 16000. 234000. 234000. 3550000. 372000. 26000. 26000. 2650. 1620. 1420. 4740. 4740. 354. 88. 255. 194. 354. 88. 261. 261. 261. 261. 261. 261. 261. 261	22. 84. 63. 115.
80. 2000. 30.	218. 218. 214. 865. 361.	75300. 154000. 2397000. 365000. 10400. 10000.	459000. 145000. 14600. 228000. 3560000. 425000. 425000. 2080000. 2080000. 2450. 47500. 47500. 2229. 213000. 26500. 1168. 2245000.	27. 74. 74. 90. 63.
60• 2000• 30•	218. 218. 75. 390. 720. 329.	94000. 142000. 249000. 720000. 72000. 5890. 17000.	379000. 412000. 5890. 2125000. 219000. 3570000. 757000. 2120000. 2120000. 2460. 1430. 47600. 15. 201. 115. 201. 115. 201. 115. 201. 115. 201. 115. 201. 115. 201. 115. 201. 115. 201. 115. 204. 2000.	31. 65. 47. 66.
40. 2000. 30.	219. 219. 75. 521. 614. 304.	108000. 133000. 236000. 137000. 614000. 2290. 2630. 35600.	2770000- 290000- 26300- 890000- 1170000- 35800000- 4880000- 3520000- 3520000- 2160000- 2160000- 2160000- 216000- 11100- 3420- 11100- 11	W W 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
20. 2000. 30.	219. 219. 75. 628. 528. 562.	117000. 126000. 239000. 45900. 528000. 1970. 660. 35900.	151000 149000 94500 1100000 3600000 3600000 389000 2170000 2170000 2170000 4290 1440 4790 117 66 99 118 117 66 99 138 118 118 118 118 118 118 118	49. 49. 38. 21.
2000.	220. 220. 75. 685. 482. 263.	121000. 121000. 241000. 482000. 1800. 0.	-683. 96500. 193000. 3610000. 510000. 508000. 1020000. 2470. 2460. 4910. 48200. 48200. 48200. 111. 111. 111. 110. 136000.	36. 36. 36. 36.
VFLOCITY, KNOTS GROSS WEIGHT, TONS CLEARANCE HEIGHT, FT	LENGTH, FT WIDTH, FT RASF PRESSURF, LB/FT*FT WETGHT OF PAYLOAD, TONS WETGHT OF POWER PLANT, TONS WETGHT OF REACTOR SHIELD, TONS WETGHT OF STRUCTURE, TONS	FRONT COMPRESSOR S.H.P. REAR COMPRESSOR S.H.P. SIDE COMPRESSOR S.H.P. THRUST COMPRESSOR S.H.P. TOTAL S.H.P. TOTAL R.A.P. AERO DYNAMIC ORAG. LB WAVE DP AG. LB	MOMENTUM DRAG, LB TOTAL DRAG, LB FORT A DRAG, LB ERR JFT LIFT, LB REAR JFT LIFT, LB SIDE JET LIFT, LB SIDE GOMPRESSOR AIR FLOW, FT**3/SEC SIDE COMPRESSOR AIR FLOW, FT**3/SEC FRONT AIR FLOW, FT**3/SEC FRONT AIR AREA, FT*FT SIDE JET AREA, FT*FT SIDE JET AREA, FT*FT SIDE JET AREA, FT*FT SIDE JET AREA, FT*FT SIDE COMPRESSOR PRESSURE DIFFERENCE, LB/FT*FT FRONT COMPRESSOR PRESSURE, LB/FT*FT FRONT NOZZLE PRESSURE, LB/FT*FT FRONT JET HFAT TRANSFER, BTU SIDE JET HFAT TRANSFER, BTU THRUST NOZZLE PRESSURE, LB/FT*FT FRONT JET HFAT TRANSFER, BTU THRUST NOZZLE PRESSURE, LB/FT*FT FRONT JET HFAT TRANSFER, BTU TOTAL JET HFAT TRANSFER, BTU TOTAL JET HFAT TRANSFER, BTU TOTAL JET HFAT TRANSFER, BTU	FULL JET TEMPERATURE RISE, DEG. F REAR JET TEMPERATURE RISE, DEG. F SIDE JET TEMPERATURE RISE, DEG. F THRUST JET TEMPERATURE RISE, DEG. F AVERAGE AIR TEMPERATURE RISE, DEG. F

TABLE I. - Continued. PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

VFLOCITY, KNDTS GROSS WEIGHT, TONS CLEAPANCE HEIGHT, FT	2000. 40.	12. 2000. 40.	24. 2000. 40.	36. 2000. 40.	48. 2000. 40.	60°- 2000°- 40°-
LENGTH, FT	216.	215.	215.	215.	214.	214.
RASE PRESSURE, LB/FT*FT	75.	75.	75.	75.	75.	75.
H _C	505	419.	400	314.	219.	101
in i	632.	655.	719.	790.	369.	381
WEIGHT OF STRUCTURE, TONS	554.	553	552.	551.	551.	550.
FRONT COMPRESSOR S.H.P.	158000.	156000.	152000.	145000.	135000.	123000.
REAR CHWPRESSOR S.H.P.	158000.	163000.	169000.	174000.	181000.	189000.
SIDE COMPRESSOR S.H.P.	316000.	314000.	312000.	310000.	310000.	343000
TOTAL S.H.P.	632000	655000	719000.	790000	869000	968000
TOTAL REACTOR POWER, MEG-W	236	2440.	2680.	2950.	3240.	3610.
AFRO DYNAMIC DRAG. LA	• •	230.	915.	2050	3640.	5670
MAVE URAGE LB	-894	-48400	-52200	-40800	-19400	10800
MOMENTUM DRAG. LB	•0	122000.	231000.	327000.	413000.	48 7000.
	-894.	90900	226000.	330000.	422000	519000
AERO DYNAMIC LIFT, LB	0.000	230.	123000	118000	3640	105000
25.30 JET 1 16T 18	127000.	141000.	147000.	153000.	158000.	165000.
SIDE JET LIFT, LB	253000.	257000.	265000.	274000.	282000.	290000
	34 90000.	3480000	3460000.	3450000.	3440000.	3440000
FRONT COMPRESSOR ATR FLOW, FT**3/SEC	668000	664000	656000	644000.	627000.	605000
KTAK CUBIKESSUK AIK TEUN TIHAS VARC	1330000	1290000	1210000.	1130000.	1040000	964000
THRUST COMPRESSOR AIR FLOW, FT**3/SEC	0	243000.	389000	478000.	549000.	618000
TOTAL AIR FLOW. FT**3/SEC	26 70000.	2740000.	2750000.	2710000.	2660000.	2610000.
FRONT LET AREA FIRET	3240.	3250	3220.	3220.	3220.	3210
KFAK JFT AKFA, FT*FT	5220.	50.50°	5290.	4550.	3890.	3300
THRUST JET AREA, FT*FT	1400.	1390	1390.	1380.	1380.	1370
TITAL AREA, FT*FT	46600.	46400*	46200.	4,6000	45900.	45800
DYNAMIC PRESSURE. 18/FT*FT	0:	0	.2.	÷ u	*	1 / 0
PRINT COMPRESSOR PRESSORT UITTERFUCE, LB/TIMTI	• · ·	110.	162	178.	194.	211.
SIDE COMPRESSOR PRESSURE DIFFERENCE, LB/FFFT	111.	114.	120.	129.	139.	151.
THRUST COMPRESSOR PRESSURE DIFFERENCE, LB/FT*FT	•0	41.	104.	157.	206.	260.
FRONT VOZZLE PRESSURT, LB/FITHET	• 66	966	96	98.	97.	9000
717 NO 77 D DEPONICATION - 10 NO 14 NO 17	100	103	110.	119.	131	146
THRUST NOZZLF PRESSURE, LB/FT*FT	0	37.	95.	145.	192.	244.
FRONT JET HEAT TRANSFER, BTU	447000.	442000	429000.	*00060*	382000.	348000
REAR JET HEAT TRANSFER, BTU	447000	460000.	477000.	493000.	512000.	535000
SIDE OF HEAT TRANSFER, BIU	9.94000	889000	882000.	8 / 8000.	877000	921000
TATAL CAL TRANSPER DEC	1790000	1850000	2030000	2230000	2460000	2740000
FRONT JET TEMPERATURE RISE. DEG. F	36.	36.	35.	34.	33.	31.
REAR JET TEMPERATURE RISE. DEG. F	36.	46.	52.	58	63	89
	36.	37.	39.	42.		7 0
THRUST JET TEMPERATURE RISE, DEG. E Aveoace ato temperature often dec. E	9.6	13.	946	51.	• 6 4	56.
	•	200	•	•) -	1

250. 3000. 10.	275.	75.	831.	354.	800	52600*	121000.	658000	3100.	163000.	1980.	000000	453000.	163000.	0	107000	*0000695	0	54200.	144000	1490000	0	77.	227.	2280.	215		453	391.	238	582.	526.	389.	o .	149000.	1860000	2350000.	Ö	147.	77.	84.
200. 3000. 10.	277.	1210.	616.	304.	*60g	49500	106000	460000	2300	105000.	2990	•00000	399000	105000.	0	105000	5750000	•0	. 00619	178000.	1360000	0	117.	343。	2300	138.	56.	341.	279.	193.	419.	363.	285.	0	140000	1300000	1740000.	0	111.	90.	. 89
150. 3000. 10.	277.	75.	539*	285.	8/I.	70700	97900.	370000.	2010	59600	5080.	139000	415000.	59600	0	62200	57.70000	0	124000.	222000.	1330000	0	258	534.	2310.	. 1000	16.	266.	206.	175.	302	248	221.	•	200000	1050000	1520000.	, 0	86.	57.5	61.
3000. 10.	278.	75.	400	245.	873.	65.300	94900	217000.	400000 1490	26600	10600.	00000	337000.	26600.	22000.	90800	\$79000°.	158000.	145000.	283000	1380000	1040	372.	875.	2320	3.6	67.	211.	157.	128.	200	169.	143.	64300	185000.	614000	1130000	22.	68°	. [4	44.
50. 3000. 10.	279.	75.	271.	202	874.	55600.	97800.	74200.	271000.	6670.	37700.	009-	192000.	6670.	36100	50200	5820000	203000	158000.	367000.	1270000	1040.	512.	1480.	2330	.0097	100	165.	125.	64.	156.	119.	65.	122000.	157000.	210000	766000.	32.	33	21.	32.
9. 3000. 10.	279.	75.	204.	175.	876.	51100.	102000	•0	204000	0	0	- 687-	-289-	•0	40300	40900	5840000	216000.	215000.	431000.	8.52000	1050	1040.	2080.	2330.	.7300		111.	111.	° į	.001	100	0	144000.	144000.	.00082		36.	36.	36.	36.
VELOCITY, KNOTS GROSS WEIGHT, TONS CLEARANCE HEIGHT, FT	LENGTH, FT MIDTH, FT	BASE PRESSURE, 18/FT*FT	WFIGHT OF PARED PONS		WEIGHT OF STRUCTURE, TONS	FRUIN COMPRINGS NATER		THRUST COMPRESSOR C.H.P.	TOTAL S.H.D. TOTAL DEACTOR DOWER. MEGW	AERO DYNAMIC DRAG, LB	WAVE DRAG. LB	JET DRAG, LB	MOMENTUM DRAG. LB	AFRO DYNAMIC LIFT. LB	FRONT JET LIFT, LB	REAR JET LIFT. LB	SIDE JET LIFT, LB	FRONT COMPRESSOR AIR FLOW, FT**3/SEC	REAR COMPRESSOR AIR FLOW, FT**3/SEC		THRUST COMPLESSOR AIR FLOW, FT**3/SEC	ROOM OF ASEA, FIRST	REAR JET AREA, FT*FT	SIDE JET AREA. FT*FT	THRUST JET AREA, FT*FT	TOTAL AREA, FT*FT	CONTRACTOR DESCRIPTION OF THE PROPERTY OF THE SET		_	THRUST COMPRESSOR PRESSURE DIFFERENCE, LB/FT*FT	FRONT NOZZIE PRESSURT, LB/FL*FL	ATOM NOZZIE PRESSURE, LB/FT#FT	THRUST NOZZLE PRESSIRE, LB/FT*FT	FRONT JET HEAT TRANSFER, BTU	REAR JET HEAT TRANSFER, BTU	SIDE JET HEAT TRANSFER, BIC	TOTAL JET HEAT TRANSFER, BTU	FRONT JET TEMPERATURE RISE, DEG. F	REAR JET TEMPERATURE RISE, DEG. F	SIDE JET FRADERATURE RISE, DEG. H	AVERAGE AIR TEMPERATURE RISE, DEG. F

TABLE I. - Continued, PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

250. 3000. 20.	272. 272. 75. 290. 1400. 458. 854.	103000. 237000. 1060000. 1400000. 5210. 159000.	400000- 731000- 159000- 84100- 210000- 5550000-	107000 286000 14100000 1800000 0 2220 73900 215 450 450 215 65000 290000 2990000 3950000 3950000 3950000
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150. 3000. 20.	273. 273. 75. 679. 1060. 400.	147000. 204000. 711000. 1060000. 3960. 57900.	400000- 734000- 57900- 130000- 203000- 561000- 236000-	236000 1160000 1160000 18100000 711 963 2240 77 16 228 228 228 228 231 414000 576000 500000 300000 94 74
100. 3000. 20.	274* 274* 75* 970* 819* 351*	44800. 195000. 195000. 445000. 819000. 25800. 10300.	454000. 605000. 25800. 43400. 121000. 193000. 5620000.	272000. 9630000. 2080000. 2080000. 2080000. 74900. 74900. 74900. 34. 67. 231. 112. 112. 127000. 381000. 551000. 1260000. 2320000. 2320000. 2320000.
50. 3000. 20.	274. 274. 274. 1375. 538. 284.	85200. 112000. 194000. 146000. 538000. 2010. 6470. 36600.	285000. 324000. 6470. 71200. 100000. 177000. 5650000.	208000 201000 654000 2060 2760 2260 75300 100 1175 101 241000 3176 101 241000 11520000 11520000 11520000
3000.	275. 275. 175. 1490. 403. 246.	101000. 101000. 202000. 403000. 1500. 0.	2570. 80600. 80800. 162000. 5680000. 426000.	425000 4700000 2060 2050 4100 75700 75700 111 111 111 111 1100 285000 285000 570000 570000 5100 1000 1140000 360
VELOCITY, KNOTS GROSS WEIGHT, TONS CLEARANCE HEIGHT, FT	LENGTH, FT WIDTH, FT MIDTH, FT RASE PRESSURE, LB/FT*FT WEIGHT OF PAYLOAD, TONS WEIGHT OF POWER PLANT, TONS WEIGHT OF STRUCTURE, TONS	FRONT COMPRESSOR S.4.P. REAR COMPRESSOR S.4.P. SIDE COMPRESSOR S.4.P. THRUST COMPRESSOR S.4.P. TOTAL S.4.P. TOTAL REACTOR POWER, MEG-W AERD DYNAMIC DRAG, LB WAVE DRAG, LB	MOMENTUM DRAG, LB TOTAL DRAG, LB AFRI DYNAMIC LIFT, LB FRONT JFT LIFT, LB REAR JFT LIFT, LB SIDE JFT LIFT, LB CUSHITM LIFT, LB FRONT COMPRESSOR AIR FLOW, FT**3/SEC REAR COMPRESSOR AIR FLOW, FT**3/SEC	

270. 270. 269. 270. 770. 270. 269. 270. 754. 1050. 171. 153. 17. 1060. 176. 171. 153. 17. 1060. 176. 176. 179. 179. 179. 1140. 176. 170. 1790. 189000. </th <th>30.</th> <th>30.</th> <th></th> <th></th> <th>• 00</th> <th>30*</th>	30.	30.			• 00	30*
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996. 754. 1050. 1510. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 1530. 154000.	1250.	1060.	708	171.	143.	29.
299, 857, 867, 846, 449, 449, 853, 850, 860, 870, 846, 844, 870, 870, 870, 870, 870, 870, 870, 870	596.	754.	1050.	1510.	1530	1630.
14900. 13400. 9320. 3440. 9320. 9320. 9320. 93200.	299.	337	397	476.	479	495
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-44, 37400, 688000, 1010000, 941000, 931 19000, 119000, 14500, 150000, 15000, 15000, 150000, 150000, 150000, 150000, 150000, 15	•	345000.	577000.	694000.	557000.	564000.
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#3/SEC	119000.	145000.	166000.	197000.	163000	129000
### 3/SEC	239000.	258000.	280000	295000	303000	309000
## 3/SEC 6430000 604000 356000 366000 366000 0 100	5520000	5480000	5450000	5430000	54 70000.	5460000
34.5EC 1260000 4440000 5360000 576000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 17500000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 1750000 175		604000	526000.	364000.	0 00	0
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##5/SEC 2510000		10,0000	844000	120000	270000	260000
## State		2780000	222000	26.20000	213000	205000
## STATE CONTRINENT OF THE CON	2050	2	3030	3030		
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ERENCE, LB/FT*FT 111. 104. 83. 448. 88. 7290. 7290. 7290. 729000. 729000. 7	6070	43.20	2670	1690	1240.	928
FERNCE, LB/FT*FT 111, 104, 83, 49, 68, 72 22, 49, 68, 19, 19, 19, 104, 83, 48, 19, 19, 111, 112, 127, 162, 214, 364, 376, 376, 19, 117, 117, 127, 162, 213, 256, 172, 162, 213, 256, 100, 110, 110, 160, 217, 234, 364, 376, 100, 110, 110, 110, 110, 110, 110, 11	2210.	2190.	2180-	2170	2190-	2180
ERENCE, LB/FT*FT 111, 104, 83, 48, 19, 88, 19, 111, 112, 127, 127, 221, 279, 321, 19, 111, 117, 127, 128, 256, 19, 19, 111, 117, 127, 128, 256, 176, 190, 117, 117, 128, 184, 197, 118, 117, 118, 117, 118, 118, 118, 11	73600	73100	72700-		72900	72800
FRENCE, LB/FT#FT 111. 104. 83. 48. 19. RENCE, LB/FT#FT 111. 173. 221. 279. 321. RENCE, LB/FT#FT 111. 173. 221. 279. 321. RENCE, LB/FT#FT 111. 173. 221. 279. 321. FERENCE, LB/FT#FT 111. 127. 162. 231. 376. FFRENCE, LB/FT#FT 111. 127. 163. 256. FT 100. 160. 160. 163. 232. 301. FT 421000. 379000. 263000. 106000. 645000. 894000. 3240 G. F 823000. 2130000. 256000. 4260000. 4320000. 45	c		22.	*6*	88	138
RENCE, LB/FT*FT 111. 173. 221. 279. 321. 256. RENCE, LB/FT*FT 111. 127. 162. 213. 256. 256. RENCE, LB/FT*FT 111. 127. 162. 213. 256. RENCE, LB/FT*FT 111. 127. 162. 213. 376. FERENCE, LB/FT*FT 111. 127. 162. 213. 376. FT 100. 160. 160. 217. 291. 360. FT 421000. 379000. 263000. 106000. 645000. 894000. 825000. 825000. 825000. 826000. 826000. 2890000. 2890000. 2890000. 2890000. 2890000. 2890000. 2960000. 2960000. 4260000. 4	111.	104.	83.	48	19.	29.
RENCE, LB/FT*FT 111. 127. 162. 213. 256. FERENCE, LB/FT*FT 0. 117. 234. 364. 376. 376. FERENCE, LB/FT*FT 0. 117. 234. 364. 376. T	111.	173.	221.	279.	321.	373.
FERENCE, LB/FT*FT 0. 117. 234. 364. 376. 376. TC NOTE: LB/FT*FT 0. 117. 234. 364. 376. 376. TC NOTE: LB/FT*FT 0. 100. 1160. 217. 291. 360. 301. 110. 163. 232. 301. 301. 110. 163. 232. 301. 301. 110. 229. 368. 409. 409. 421000. 421000. 421000. 421000. 421000. 535000. 645000. 645000. 8944000. 1690000. 2130000. 2960000. 421000. 2960000. 4260000. 4320000. 3240. 134. 27. 15. 0. 104. 6600	111.	127.	162.	213.	256.	309
T 99. 98. 92. 83. 88. 88. 100. 160. 160. 217. 291. 360. 360. 100. 160. 217. 291. 360. 360. 100. 110. 229. 368. 409. 409. 110. 229. 368. 409. 409. 421000. 421000. 224000. 535000. 645000. 645000. 645000. 234000. 2130000. 2240000. 2240000. 2240000. 2240000. 2240000. 2240000. 2240000. 2260000. 4200000. 4200000. 4200000. 420000. 420000. 420000. 420000. 420000. 420000. 420000. 420000. 420000. 420000. 420000.	.c	117.	234.	364.	376.	394.
FT 100. 160. 217. 291. 360. 360. 110. 119. 163. 232. 301. 301. 110. 229. 348. 409. 37000. 379000. 263000. 106000. 645000. 645000. 823000. 134000. 2964000. 2964000. 2964000. 2964000. 2960000. 2960000. 2960000. 2960000. 2960000. 2960000. 2960000. 2960000. 4260000. 4260000. 4320000. 45000. 6600. 6600. 690. 690. 104. 56. 71. 90. 118. 122. 691. 83. 691. 691. 83. 691. 691. 691. 691. 692. 691. 691. 691. 691. 691. 691. 691. 691	•66	•86	92.	83.	88.	138.
FT 100, 119, 163, 232, 301, 409, 100, 110, 2229, 368, 409, 409, 110, 2229, 368, 409, 409, 110, 2229, 368, 409, 433, 421000, 379000, 263000, 645000, 825000, 825000, 825000, 825000, 825000, 825000, 826000, 2890000, 294000, 2940000, 2940000, 4260000, 432000, 46000, 6600, 6	100	160.	217.	291.	360	447.
42100. 37900. 26300. 106000. 0. 409. 42300. 451000. 379000. 263000. 106000. 535000. 4333 4621000. 845000. 845000. 843000. 825000. 867000. 894000. 934 825000. 867000. 2890000. 3240 934 825000. 2130000. 2960000. 4260000.	100.	119.	163.	232.	301.	390.
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843000, 823000, 825000, 867000, 894000, 934 0, 468000, 1340000, 2640000, 42890000, 3240 36, 36, 71, 90, 104, 36, 41, 52, 69, 83, 122,	421000.	462000.	531000.	645000	535000	433000
0. 468000. 1340000. 2640000. 2890000. 3240 1690000. 2130000. 2960000. 4260000. 4320000. 4600 36. 28. 71. 90. 104. 36. 41. 52. 69. 83. F 36. 41. 58. 87. 109.	843000.	823000.	825000.	867000.	894000	934000
1690000, 2130000, 2960000, 4260000, 4320000, 4600 36, 34, 27, 15, 90, 104, 36, 41, 52, 69, 83, F 36, 41, 58, 87, 109,	0	468000	1340000.	2640000.	2890000	3240000
36. 34. 27. 15. 0. 36. 56. 71. 90. 104. 36. 41. 52. 69. 83. F 36. 41. 58. 87. 109.	1690000	2130000.	2960000	4260000.	4320000	4600000
36. 56. 71. 90. 104. 36. 41. 52. 69. 83. F 0. 38. 76. 118. 122. F 36. 41. 58. 87. 109.	36.	34.	27.	15.	0	0
F 0. 38. 76. 118. 122. F 36. 41. 58. 87. 109.	36.	56.	11.	906	104.	121.
F 0. 38. 76. 118. 122. F 36. 41. 58. 87. 109.	36.	41.	52°	*69	83.	100.
F 36° 41° 58° 87° 109°	ć	38.	76.	118.	122.	128.
	36.	41.	e ec	87.	100	120.
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TABLE I. - Continued. PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

VELOCITY, KNOTS GROSS WEIGHT, TONS CLEARANCE HEIGHT, FT	0 3000 40°	18. 3000. 40.	36. 3000. 40.	54. 3000. 40.	72. 3000. 40.	90° 3000° 40°
LENGTH, FT	268.	267.	266.	266.	266.	265
WIDTH, FT BASE DRESSIDE, 19/FTSET	75.	75.	75.	75.	75.	75.
WEIGHT OF BAYLDAD, TONS	1030.	996	806	635.	403	119.
	784.	840.	974.	1120.	1320.	1560
WEIGHT OF REACTOR SHIELD. TONS	343.	600 800 800 800	9 00 00 00 00 00 00 00 00 00	410	835.	3000
	196000	192000	180000	161000.	135000	105000.
REAR COMPRESSOR S.H.P.	196000.	204000	215000.	227000.	243000	264000
SIDE COMPRESSOR S.H.P.	392000	388000	384000	383000	387000.	396000
THRUST COMPRESSOR S.H.P.	784000	840000	974000	1120000	1320000	1560000
TOTAL REACTOR POWER, MEG-W	2920	3130	3630	4170.	4910.	5820.
AERO DYNAMIC DRAG, LB	•	794.	3160.	7100.	12600.	19600.
WAVE DRAG LB	-1110-	32600°-	63000	-4260	63 900	155000
MOMENTUM DRAG, LB	0	222000.	410000.	567000.	.000 \$69	793000
TOTAL DRAG, LB	-1110.	194000	428000.	•000009	788000	979000
AERO DYNAMIC LIFT, LB	157000	154000	147000	135000	119000	97700
REAR CET FATTA ES	157000.	1.78000.	189000	200000	213000.	228000.
SIDE JET LIFT. LB	314000.	323000	338000	353000	366000	377000.
C + + + + + + + + + + + + + + + + + + +	53 70000	5340000	5320000	5310000.	22.90.000	•000003c
PRON- COMPRESSOR AIR FLUX. THRESTOR	826000.	642000	578000.	542000	516000.	499000
SIDE COMPRESSOR AIR FLOW, FT**3/SEC	1650000	1570000.	1420000.	1270000.	1130000.	1010000
THRUST COMPRESSOR AIR FLOW, FT**3/SEC	0	448000.	682000	829000	969000	1100000.
TOTAL AIR FLOW, FT##3/SEC	3310000.	3480000	34 (0000°-	3410000	3330000	3980
ACIDA DATA ACIDA TINETI	3990	2340	1840.	1560.	1350.	1190
SIDE JET AREA, FT#FT	7980.	7130.	5770.	4610.	3650.	2910.
THRUST JET AREA, FT#FT	2150.	2140.	2130	2120.	2120-	2110.
TOTAL AREA, FT*FT	71600.	71300.	-00017	-0000	.0200	70400
DYNAMIC PRESSURE, LS/FIRTI FRONT COMPRESSOR DRESSING DIFFERENCE, LB/FIRFI	111.	109.	105.	* 86 6	 	75.
RESSURE DIFFERENCE, L	111.	149.	174.	196.	221.	248.
MPRESSOR PRESSURE DIFFERENCE, LB	111.	116.	127.	141.	160.	183
THRUST COMPANISON PRESSURE DIFFERENCE, LB/FI*FI	• 6	\$ 00	134	196	9007	900
PRONI NOZZEN PRESSURTO LOJINET PERA NOZZE POPENCIPE, IRJETART	100	135	160.	185	213.	246.
SIDE NOZZLE PRESSURE, LB/FT*FT	100.	105.	118.	135.	159.	187.
THRUST NOZZLE PRESSURE, LB/FT*FT	0	53.	124.	184.	253	327.
FRONT OF THEAT TRANSPER, BTC	554000	542000	508000	*2000°	20000	.000147
REAR JET HEAT TRANSFER, BIU	1110000	1100000.	1090000	1080000	1090000	1120000
THRUST JET HEAT TRANSFER, BTU	•0	157000	551000.	982000	1560000.	2250000.
	2220000.	2370000.	2750000.	3160000.	3720000	4420000
FRONT JET TEMPERATURE RISE, DEG. F.	36.	35.	 9:00 	32.	28.	24.
REAR JET TEMPERATURE RISE, DEG. F.	9 9	* & &	500	6 4 6 4	5.25	
THREAT INTITUTE ATTEMPT ATTEMP	° °	19.	• • • • • • • • • • • • • • • • • • •	63.	86.	110.
AVERAGE AIR TEMPERATURE RISE, DEG. F	36.	37.	42.	50°	•09	73.
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VELOCITY, KNOTS GROSS WEIGHT, TONS CLEARANCE HEIGHT, FT	3000° 50°	3000. 50.	26. 3000. 50.	3000° 3000° 50°	52. 3000. 50.	65. 3000. 50.
ENGTH, FT	264.	263.	263.	262.	262.	262.
BASE PRESSURE LB/FT*FT	75.	75.	75.	75.	75.	75.
WEIGHT OF BAYLOAD, TONS	822.	779.	. 929	2009	344.	140
OF.	967.	1000.	1110.	1240.	1380.	1550.
	381.	386	*00°	451.	400°	30 C
MEIGHT OF STRUCTURE, TONS	830.	230000	. 921000	*C28	901000	179000
TRONE COMPRESSION Name of the contract of the	242000	249000	259000.	269000	281000	296000
ATOM COMPANY ALL D.	483000	480000	476000.	474000.	475000.	480000
THRUST COMPRESSOR S.H.P.	•0	35700.	143000.	274000.	420000	599000
TOTAL S.H.P.	967000	1000000	1110000.	1240000	1380000	1550000
TOTAL REACTOR POWER, MEG-W	3600.	3740.	4130.	4600*	5150	9790
AERO DYNAMIC DRAG, LB	• c	*60%	1010.	5.2800.	31200	20800
MAVE DRAG LB	-1370.	-75000	-77700	-55800	-16000	39300
ADERICA DRAG. 1.8	0	201000.	379000	534000	6 70000.	78 5000.
TOTAL DRAG, LB	-1370.	147000.	358000.	535000	691000	855000
AERO DYNAMIC LIFT, LB	.	403.	1610.	3600	6380.	9940
	193000.	191000.	187000.	179000.	1,68000	154000
REAR JET LIFT, LB	194000.	20,000	226000.	236000	245000	25 7000°
SIDE JET LIFT, LB	5230000	520000	5180000	516000	5140000	513000
COSTION LITTO LD FIRE, FT##3/AFC	102000	1010000	1000000	979000	949000	909000
AFAR COMPRESSOR AIR FLOW, FT**3/SEC	102000	816000.	738000	*000069	657000	63.1000.
SIDE COMPRESSOR AIR FLOW, FT**3/SEC	2040000	1970000.	1830000.	1690000.	1550000.	1420000.
COMPRESSO	0	379000	601000	747000	863000	972000.
	4080000	.000014	4170000.	4110000	*050000*	3930000
PERONI JET AREA, FIRET	4920	3080	2480	2130	1880	1680.
CADE DEL ABEA. FIRET	9840	9150	7900	6680	5610.	4690
THRUST JET AREA, FT*FT	2090.	2080	2070-	2060	2060.	2050
TOTAL AREA, FT*FT	69700	.00669	•00069	68800.	68600	68400.
	o ,	- :	2.	, ,	* 6	. 4.
	• 7 7 7	110.	807	* 0.	* 6 C	* 7 6
REAR COMPRESSOR PRESSORE DIFFERENCE, LB/FI*FI	111.	145	121	131	1630	.58.
w	.0	44	1110	171.	228	288.
NOZZLE PRESSURE, LB/FT*FT	•66	*66	•66	-86	96	95°
REAR NOZZLE PRESSURE, LB/FT*FT	100.	129.	150.	168.	188.	209.
SIDE NOZZLE PRESSURE, LB/FT*FT	100	103.	111.	122.	136.	154.
THRUST NOZZLE PRESSURE, LB/FT#FT	0000	•04	102.	158.	.212	*172
FRONT JET HEAT TRANSFER, BTU	683000	674000	652000	616000.	567000	.000.0c
REAR JET HEAT TRANSFER, BIU	13 20000	1340000	1350000	1340000	1340000	136000
SIDE CEL TEAL LANGERS DIC	*00001cT	101000	404000	774000-	119000	1 690000
TOTAL SET HEAT TRANSFER. BTU	2730000	2840000	3130000	3490000	3890000	439000°
FRONT JET TEMPERATURE RISE. DEG. F	36.	36.	35.	34.		30.
REAR JET TEMPERATURE RISE, DEG. F	36.	46.	53.	59.	65.	71.
SIDE JET TEMPERATURE RISE, DEG. F	36.	37.	30°	42.	46.	21.
THRUST JET TEMPERATURE RISE, DEG. F Avedage ato temperature rise, deg. e	° 4	14.	36.	4 50 50 50 50 50 50 50 50 50 50 50 50 50	74.	. 60.90 . 00.90
AVERAGE AIR TENTENMIONE NIGHT DEG. F	5	2	• •)) }	,

TABLE I. - Continued. PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

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4000. 20.	319. 319. 75. 2110.	467. 265. 1160.	117000.	467000. 1740.	0.00	0.	93400	187000.	494000	984000.	1970000	2390	4760.	3050.	•	-11.	1111.	• 66	100	100.	330000	330000	•000000	1320000.	36.	36.	36.
VELOCITY, KNOTS GRNSS WEIGHT, TONS CLEARANCE HEIGHT, FT	LENGTH, FT WIDTH, FT BASF PRESSURE, LB/FT*FT WEIGHT OF PAYLOAD, TONS	WEIGHT OF PHWER PLANT, TONS WEIGHT OF REACTOR SHIELD, TONS WEIGHT OF STRUCTURE, TONS	FKUNI CUMPRESSIR S.H.P. REAR COMPRESSIR S.H.P. SIDE COMPRESSIR S.H.P.	THRUSI CUMPRESSUR S.H.P. TOTAL S.H.P. TOTAL REACTOR POWER, MEG-W	AFRO DYNAMIC DRAG, LB MAYF DRAG, LB	MOMENTAL DRAG. LB	AERO DYNAMIC LIFT, LB FRONT JET LIFT, LB	REAR JET LIFT, LB	FRONT COMPRESSOR AIR FLOW, FT**3/SEC	REAR COMPRESSOR AIR FLOW, FI**3/SEC	THRUST COMPRESSOR ATR FLOW, FT**3/SEC	FROM JET AREA, FT*FT DEAD IST AREA, ET*FT	SIDE JET AREA FIRET	THRUST JET ARFA, FT*FT TOTAL ARFA, FT*FT	DOWAMIC PRESSURE, LB/FT*FT		PRESSURE DIFFERENCE.	THRUST CHMPRESSOR PRESSORE DIFFERENCE, LB/FL#FL FRONT NOZZLE PRESSURE, LB/FT#FT	REAR NOTTLE PRESSURF, LB/FT*FT	SIDE NOZZLE PRESSURF, LB/FT*FT	FRONT JET HEAT TRANSFER, BTU	RFAR JET HEAT TRANSFER, BTU	THRUST JET HEAT TRANSFER, BIU		FRONT JET TEMPERATURE RISE, DEG. F		THRUST JET TEMPERATURE RISE, DEG. F AVERAGE AIR TEMPERATURE RISE, DEG. F

TABLE I, - Continued. PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

240. 4000. 30.	312.	75.	2220	578.	1130.	0	1 76000.	1640000	2220000	8290.	193000.	201000	679000	1170000.	193000.	o	144000.	7300000	0	189000.	505000	1920000.	.0000142	0.277	820.	2920.	97400.	.861	42.	45 f a	400	198.	554.	498	.126	000007	1140000	4640000	6290000	•	142.	130	129.	
192. 4000. 30.	313.	75.	1840.	526.	1140.	0	178000.	129000-	1840000	6870.	125000.	*0604 *14000	658000.	1100000	125000.	•0	153000.	73 70 000.	0	236000.	604000	1730000.	25 70000.	0 0	1170	2950	98200.	127.	27.	333°	349.	127.	450.	363.	• · ·	• 000 00	1060000	3650000	5210000.	o ;	114.	1.24	109.	
144. 4000. 30.	312.	75.	2040.	554.	1130.	7020	296000.	1370000	2040000	7610.	69600	6860.	776000	1360000	•00969	6710.	255000.	7320000	160000	454000	708000.	1690000	3010000.	3520.	1610	2930	97600.	71.	20.	305	381.	76.	333.	273.	10401	19800	1030000	3890000	5770000.	7.	99.	. 22	103.	
96. 4000. 30.	313.	75.	1390.	457	1140.	83300	232000.	734000	1390000	1	31100	14400	750000	000696	31100.	19400.	205000.	7350000	552000	458000	•000906	1350000.	3270000.	3520.	1110.	2940	•00086	32.	70.	231.	254	89.	239.	184.	2555	230000	962000	2080000	3930000.	23.	77.	٥/ د	64.	
48. 4000. 30.	314.	75.	916	372.	1140.	148000.	193000	335000.	919000	3430.	7810.	51100.	* 14900 * 4 8000	512000.	7810.	123000.	172000.	7390000	689000	506000	1200000.	921000.	3310000.	3530	1560	29 60	98600	80	101.	1.31	123.	.76	167.	124.	117.	419000°	949000	685000	2600000.	33.		45°	42.	
4000. 30.	315.	15.	1840.	323.	1140.	173000.	173000.	346000	692000	2580.	o ,	000	• 0061	-980	0	138000.	139000.	7450000-	732000.	730000	1460000.	•0	2920000	3550	3520	2980	99300	•0			• 0	•66	100.	100.	•0	489000	489000	0	1960000.	36.	36.	90.	36.	
VFL nCITY, KNOTS GRNSS WEIGHT, TONS CLEARANCE HEIGHT, FT	LENGTH+ FT WIDTH+ FT	BASE PRESSURE, LB/FT*FT	WEIGHT OF PAYLOAD, TINS		WEIGHT OF STRUCTURE, TONS	FRONT COMPRESSOR S.H.P.	REAR COMPRESSIR S.H.P.	STOE COMPRESSOR S.F.P.	HORADAL CHARLANDAR SANANA	TOTAL REACTOR POWER. MEG-W	AFRI DYNAMIC DRAG. LA	MAYE ORAG. LB		TOTAL DRAG. 18	AFRO DYNAMIC LIFT. LB	FRONT JET LIFT. LB	REAR JET LIFT. 19	SIDE JET LIFT. LB	A 10 ELOW - FT##3/	REAR COMPRESSOR AIR FLOW, FT+*3/SEC	SIDE COMPRESSOR AIR FLOW. FT**3/SEC	THRUST COMPRESSOR ATR FLOW. FT**3/SEC	TOTAL AIR FINN, FT**3/SEC	FRONT JET AREA, FT*FT	ATAK JET AKEA, THEFT	THREAT THE AREA THREE	TOTAL BRIDE FIXER	18 /FT*FT	FRONT COMPRESSOR PRESSURE DIFFERENCE, LB/FT*FT	REAR COMPERSOR PRESSURE DIFFERENCE, LB/FFFFF	· Z		REAR NOZZLF PRESSURF. LB/FT*FT	SINE NOZZLE PRESSURE, LB/FT*FT	THRUST NOTZLE PRESSURE, LB/FT#FT	FRONT JET HEAT TRANSFERS BIO	CIDE SET HEAT TRANSFIR BIU	THRUST JET HEAT TRANSFER, BTU	TOTAL JET HEAT TRANSFER, BTU	FRONT JET TEMPERATURE RISF. DFG. F	REAR JET TEMPERATURE RISE, DEG. F		THRUST JET TEMPERATURE KINE, DEG. F AVERAGE AIR TEMPERATURE RINE, DEG. F	

125. 4000. 40.	308. 308. 308. 75173. 2450. 46400. 46400. 1580000. 2450000. 1050000. 1050000. 1050000. 11900. 2370. 2850. 984000. 1190. 2370. 2370. 238. 438. 131000. 133000. 438000.	96. 74. 138. 98.
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VFLOCITY. KNOTS GROSS WFIGHT, TONS CLFARANCE HEIGHT. FT	FT SSURE, LB/FT* F PAYLOAD, TO F POWER PLAN I F REACTOR SHI AVER STOR SHI AVER SSOR SHI BY AVER SSOR SHI BY AVER SSOR SHI BY AVER SSOR AVER SOR AV	REAR JET TEMPERATURE RISE, DEG. F SIDE JET TEMPERATURE RISE, DEG. F THRUST JET TEMPERATURE RISE, DEG. F AVERAGE AIP TEMPERATURE RISE, DEG. F

TABLE I. - Continued. PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

CLEARANCE HEIGHT. ET I FNGTH. ET	308.	50.	306.	50.	50.	50.
	308	307	306.	306.	305	305
BASE DRESSURE, LB/FT*FT	1340	1280.	1080	75.	607.	75.
WEIGHT OF POWER PLANT, TONS	1130.	1190	1350.	1530.	1770.	2060.
SHIELD. TONS	412.	423.	451.	480.	516.	556.
OF STRUCTURE, TONS	•0211 •0200	•0111	243000	1110.	211000	175000
TACON TO COMPANY OF THE PARTY O	282000.	292000.	306000	321000	340000	365000
SIDE COMPRESSOR S.H.P.	563000.	559000	553000.	551000.	555000	564000.
COMPRESSOR S.H.P.	0	. 00400	231000.	422000.	662000	954000
TOTAL S.H.P.	1130000.	1190000.	1350000.	1530000.	•00007.7	-0000002
TOTAL KRACIUK PURKK. BIGHR	•002+	. 00 H	3300	7410.	13100.	20500
7* LG	• •	28500	78000.	48500	28700	19100
	-1590.	-88400	- 79300.	-32400.	42700.	145000.
MOMENTUM DRAG. 1.8	0	286000.	\$31000.	741000.	916000.	1060000.
	-1280.	227000.	533000	765000.	1000000	1240000.
AERO DYNAMIC LIFT. LB	0	829.	3300	7410.	13100	20500
FRONT JET LIFT. LB	225000	222000.	214000.	200000	182000	158000
ARAN JET LIFT. LA	226000	254000.	268000.	501000	51 9000	534000
SIDE JETT LE	7100000	1060000	7030000	7010000.	*0000669	6970000
A TR FLOW, FT**3/SEC	1190000	1180000.	1160000.	1120000.	1060000	992000.
AIR FLOW. FT**3/SEC	1190000.	935000.	841000.	789000.	749000.	722000.
SIDE CHMPRESSOR AIR FLOW, FT*#3/SEC	23 70000.	2270000.	2080000	1880000.	1700000.	1530000
DR AIR FLOW, FT**3/SEC	• 0	555000	868000	1000000	1240000	1400000
A 4 FL(JW+ F ** 3/5/5 157 A3 6 6 4 5 4 5	• 0000c1 +	4940000 5760	*340000 \$740.	5730	5730	5720
	5740	3460	2740.	2340.	2030	1800.
SIDE JET AREA. FIRET	11500.	10400	8660	7070.	5720.	4640.
THRUST JET AREA, FT#FT	2840	2820.	2810.	2800.	2800	2790.
TOTAL AREA. FT*FT	94600	94200.	93800	93500	93200	93000
LB/FT*FT	o i		* ;	.	1.4.	22.
٠	1111	•601	106.	101	93.0	320
PRESSORE DIFFERENCE.		140.	170.	190	152	173
SIDE COMPANION PARASSORE DIFFERENCES ENTRIFFERENCES CONTRACTOR DESCRIPER DIFFERENCES ENTRIFFERENCES ENTRIFFEREN	.0.	51.7	125.	186.	250*	319.
į	66	*66	98	97.	95.	92.
SSURE, LB/FT#FT	100	132.	156.	178.	202	230.
SIDE NOZZIE PRESSURF. LB/FT*FT	100	104.	115.	130.	149.	173.
THRUST NOZZI E PRESSURF, LB/FT*FT	0	47.	115.	173.	237.	305
FRONT JET HEAT TRANSFER, RTU	796000.	782000.	743000.	681000.	\$ 57000.	496000
RFAR JFT HEAT TRANSFFR, BTU	196000.	8 2 6 0 0 0 •	864000	90700	962000	1030000
SIDE JET HEAT TRANSFER, BTU	1590000.	1580000.	1560000.	1560000.	1570000.	1590000
THRUST JET HEAT TRANSFER, BTU	• 0	171900.	654000	1190000	18 70000	2 70000
	3190000.	3360000	3830000	4340000.	2000000	•000028¢
RISE, DEG.	36.	35.	34.	433	•00	. 12
ATEA CIT TREPERS TATE OF THE CONTROL	96	27.	• 66	• 70	• C	- 10
	• 00	. 71	• • • •	• •		103.
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TABLE I. - Continued. PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

VFLOCITY, KNOTS CARDES GROSS WFIGHT, TONS CLEARANCE HEIGHT, FT	5000° 5000°	50° 5000• 20•	100. 5000. 20.	150. 5000. 20.	200. 5000. 20.	250. 5000. 20.
LENGTH, FT WIDTH, FT BASE PRESSURE, LB/FT*FT WFIGHT OF PAYLDAD, TONS	357. 357. 75. 2750.	357. 357. 75.	356. 356. 75. 2120.	355. 355. 75. 1740.	355. 355. 75. 1620.	353° 353° 75° 1140°
	524. 281.	694. 323. 1450.	.1040. 396.	1370. 454. 1440.	1470. 471. 1440.	1900. 534. 1430.
FRONT COMPRESSOR S.H.P. REAR COMPRESSOR S.H.P. SIDE COMPRESSOR S.H.P.	131000.	111000.	58200. 172000. 249000.	0. 186000. 259000.	0. 128000. 275000.	134000. 306000.
THRUST COMPRESSOR S.H.P. TOTAL S.H.P. TOTAL DEACTOR DOWER, MEC.L.	524000 1950	187000.	565000. 1040000.	924000. 1370000. 5100.	1470000.	1460000.
AERO DYNAM IC DRAG. LB	0.0	10900.	43500.	97700.	173000.	268000.
JHT DRAG. LH JHT DRAG. LB TOTAL DRAG. LB	-741. 0. -741.	374000. 442000.	599000. 599000. 811000.	524000. 529000. 990000.	532000. 510000. 921000.	521000. 521000. 1010000.
AFRO DYNAMIC LIFT. LB FRONT JET LIFT. LB	105000	10900.	43500.	\$7700°	173000.	268000.
REAR JET LIFT, LB SIDE JET IFT, LB	210000.	129000° 229000°	250000.	169000. 263000.	270000.	273000.
FOUNT CIPTOLD FRONT COMPRESSOR PEAN COMPRESSOR AT FIRM FT**3/SEC	553000.	519000.	405000.	0.0001	.0000	140000
THRUST COMPRESSOR AIR FLOW, FT**3/SEC	1100000.	922000.	704000.	554000.	453000.	372000.
	2210000.	2850000.	2960000.	.0000892 0.	2620000.	2780000.
RFAR JET ARFA, FT*FT SIDE JET AREA, FT*FT	2670.	1250.	898.	634.	296. 869.	588.
THRUST JFT AREA, FT*FT TOTAL AREA, FT*FT	3830. 1.28000.	3820. 127000.	3800. 127000.	126000.	3780.	3740. 125000.
TC PRESSURE, L9/FT*FT COMPRESSOR PRESSURE DIFFERENCE,	0. 111.	100.	34. 67.	17.	138. 29.	215.
ய ய	· · · · · · · · · · · · · · · · · · ·	171.	223.	280.	286.	386.
THRUST COMPRESSOR PRESSURE DIFFERENCE, LB/FI*FT FRONT NOTZLE PRESSURE 18/FI*FT	•66	97.	88.	77.	138.	215.
REAR NOTZLE PRESSURE, L97F18F1 STOF NOTZLE PRESSURE, L97F18F1 TUDIET MOTZLE PRESSURE, L07F18F1	1001	161.	177.	259.	367.	521.
FRINT JET HEAT TRANSFER, BTU REAR JET HEAT TRANSFER, BTU		313000.	164000.	526000	362000	378000
SIUP JET HEAT TRANSFER, BTU THRUST JET HEAT TRANSFER, BTU TOTAL JET HEAT TRANSFER, BTU	1480000.	530000. 530000. 1960000.	1600000.	2610000. 3870000.	3030000. 4170000.	4120000. 5370000.
FRONT JET TEMPERATURE RISE, DEG. F REAR JET TEMPERATURE RISE, DEG. F KIDE JET TEMPERATURE BISE, DEG. E	. 36. 36. 36.	32. 55.	72.	91.	0. 112. 92.	145.
THRUST JET TEMPERATURE RISE, DEG. F AVERAGE AIR TEMPERATURE RISE, DEG. F	36.	28.	95.2	77.	88.8	97.

250. 5000. 30.	350. 350. 311. 2640. 2640. 460000. 1420. 26300. 26300.	125 . 126.
200° 5000° 30°	351. 351. 75. 881. 2130. 1430. 149000. 1510.000. 2130.000. 170000. 1750. 1750. 1750. 1750. 1760. 1770. 1780. 17	105.
150. 5000. 30.	351. 351. 75. 2060. 2060. 399000. 1380000. 2060000. 76900. 76000. 76000. 76000. 76000. 76000. 76000. 76000. 77	104• 96•
100. 5000. 30.	351. 75. 1480. 1600. 26200. 380000. 380000. 6700. 67000. 6700. 6700. 1150000. 6700. 866000. 115000. 115000. 115000. 11500. 1150. 1	79.
50. 5000. 30.	352. 2130. 1040. 1040. 2170. 2170. 2170. 2850. 107	38. 41.
5000.	354. 354. 777. 1430. 194000. 387000. 387000. 777000. 2900. 155000. 155000. 3880. 3980. 3980. 3980. 3980. 111000. 1111.	36.
VELDCITY, KNG15 GROSS WEIGHT, TONS CLEARANCE HFIGHT, FT	HENGTH, FT WIDTH, FT WIDTH ENDYESSURE, LR/FTLD, TONS WITHTOF REACTOR SHILLD, TONS WITHTOF REACTOR SHILD, FARNIT COMPRESSOR S.H.P. FIND COMPRESSOR S.H.P. FOR S.H.P. F	THRUST JET TEMPERATURE RISE, DEG. F AVERAGE AIR TEMPERATURE RISE, DEG. F

TABLE I. - Concluded. PARAMETRIC STUDY OF LARGE NUCLEAR SURFACE EFFECTS MACHINE

VFLOCITY, KNOTS GROSS WEIGHT, TONS CLEARANCE HEIGHT, FT	5000° 40°	40. 5000. 40.	80. 5000. 40.	120. 5000. 40.	160. 5000. 40.	200. 5000. 40.
LENGTH, FT WIDTH, FT RASE PRESSURE, LB/FT*FT WEIGHT OF POWER PLANT, TONS	350. 350. 75. 2160. 1020.	349. 349. 75. 1850. 1300.	348. 348. 75. 1260. 1810.	347. 347. 75. 367. 2600.	348. 348. 75. 324. 2630.	348. 348. 75. 140. 2800.
	393 1420 256000 256000 512000	442. 1410. 230000. 281000. 500000.	521. 1410. 160000. 323000. 502000.	625. 1410. 64300. 393000. 529000.	629. 1410. 0. 326000. 546000.	649. 1410. 0. 264000. 570000.
THRUST COMPRESSOR S.H.P. TOTAL S.H.P. TOTAL REACTOR POWER, MEG-W AFRO DYNAMIC DRAG, LR WAVE DRAG, LR JET DRAG, LR MOMENTUM DRAG, LR	1020000 3820. 3820. 0. -1450. 0.	284000- 1300000- 4830- 6690- 86800- -49500- 592000-	820000 1810000 6730 2660 24500 137000 989000	1610000 2600000 9690 59600 11700 1190000 1730000	1760000- 2630000- 9820- 107000- 6960- 576000- 955000- 1640000-	1970000. 2800000. 10400. 167000. 45400. 453000.
AFRO DYNAMIC LIFT, LB FRONT JFT LIFT, LB REAR JFT LIFT, LB SIDE JET LIFT, LB CUSHION LIFT, LB FRONT COMPRESSOR AIR FLOW, FT**3/SEC	205000. 205000. 205000. 411000. 9180000.	6690. 189000. 249000. 444000. 9110000. 1040000.	26600. 144000. 286000. 482000. 9060000.	59600. 69000. 338000. 507000. 9030000. 666000.	107000. 0. 280000. 522000. 9090000.	167000. 0. 222000. 531000. 9080000.
##3/5 FT##3/5 FEREN PEREN FET FFT FFT FFT	2160000. 4320000. 5250. 10400. 3670. 112000. 111. 111. 111. 111. 111. 111.	1830000. 1740000. 5230. 2420. 7410. 3640. 121000. 121000. 1210. 173. 173. 128. 120. 161. 119.	1450000 1600000 46300000 1760 1760 121000 121000 22 83 22 22 162 240 240 240 240 240 240 240 24	1150000 2020000 44500000 5210 1400 120000 120000 49 48 281 281 215 374 83 234 182000	2140000- 21400000- 3600000- 888- 2120- 3640- 121000- 19- 323- 257- 388- 385- 88- 385- 385- 418-	2857000 3460000 3460000 0 1590 121000 1230 138 29 311 404 138 449 391 475
RFAR JFT HFAT TRANSFER, BTU SIDE JET HEAT TRANSFER, BTU THPUST JET HFAT TRANSFER, BTU TOTAL JET HEAT TRANSFER, BTU FRONT JET TEMPERATURE RISF, DEG. F REAR JET TEMPERATURE RISF, DEG. F SIDE JET TEMPERATURE RISF, DEG. F THRUST JET TEMPERATURE RISF, DEG. F AVERAGE AIR TEMPERATURE RISE, DEG. F	724000. 1450000. 2900000. 36. 36. 36. 36.	796000. 1410000. 804000. 3670000. 367. 56. 41.	915000. 1420000. 2320000. 5110000. 77. 78.	1110000. 1500000. 4560000. 7350000. 15. 91. 70. 121.	922000. 1540000. 4980000. 7450000. 0. 105. 83.	747000. 1610000. 5560000. 7910000. 0. 122. 101. 131.

100. 5000. 50.	343. 343. 75. 200. 2760.	645. 140000. 140000. 448000. 648000. 1530000. 2760000. 40500.	15900. 350000. 1350000. 176000. 136000. 384000. 616000.	8820000. 795000. 1550000. 5250000. 5250000. 11830. 4200. 13830. 118000. 1270000. 1270000. 1830000. 7810000. 7810000. 7810000. 85. 85. 85.	
80. 5000. 50.	343. 343. 75. 733.	586. 1390. 198000. 407000. 630000. 1050000. 2290000. 8530.	23900- 165000- 120000- 120000- 26000- 178000- 354000- 599000-	8840000 8230000 1740000 1740000 5380000 2080 2080 118000 22 22 23 23 24 118000 25 27 27 27 27 27 27 27 27 27 27	
60. 50.00.	344. 344. 75. 1170.	535. 1400. 247000. 374000. 620000. 1900000. 14600.	2 10000. 2 10000. 107000. 14600. 2 10000. 3 2 9 0 0 0. 5 7 7 0 0 0.	8870000. 1220000. 1980000. 1980000. 2420. 2420. 2420. 2420. 118000. 118000. 118000. 118000. 118000. 118000. 118000. 118000. 118000. 118000. 118000. 118000. 118000. 1180000. 1180000. 1180000. 1180000. 1180000. 1180000.	1
40. 5000. 50.	344. 344. 75. 1490. 1610.	493. 1400. 284000. 351000. 620000. 359000. 1610000. 6020.	64900 -65100 755000 75000 6530 6530 53000 551000	8900000 12800000 22400000 11800000 5620000 89400 89400 1190000 1190000 129 129 129 129 129 120 120 120 120 120 121 121 121 124 121 124 121 124 121 124 121 124 124	b
20. 5000. 50.	345. 345. 75. 1780. 1370.	454. 1400. 308000. 331000. 627000. 101000. 1370000.	40700 40700 397000 397000 340000 1640 248000 589000 840000	8940000. 1320000. 2510000. 5640000. 3716. 11300. 11	
50005	346. 346. 75. 1890.	437. 1400. 317000. 317000. 634000. 1270000.	-1790 -1790 -1790 -1790 -254000 -254000 -254000	8980000 1340000 1340000 2670000 6450 6450 129000 129000 111 111 111 100 896000 179000 17	;
VFLOCITY, KNOTS GRDSS WFIGHT, TONS CLEARANCE HEIGHT, FT	LENGTH, FT WIDTH, FT BASE PRESSURE, LB/FT*FT WEIGHT OF PAYLOAD, TONS WEIGHT OF PIWER PLANT, TONS	WEIGHT OF REACTOR SHIFLD, TONS WEIGHT OF STRUCTURE, TONS FRONT COMPRESSOR S.H.P. REAR COMPRESSOR S.H.P. SIDE COMPRESSOR S.H.P. TOTAL S.H.P. ACON COMPANIES OF S.H.P.	WANT TANALL DRAWS 15 WANT TORAGE LB JET DRAGE LB MOMENTUM DRAGE LB TOTAL DRAGE LB AFRO DYNAMIC LIFT, LB FRONT JET LIFT, LB REAR JET LIFT, LB SIDE JET LIFT, LB	CUSHION LIFT, LA FRONT COMPRESSOR AIR FLOW, FT**3/SEC REAR COMPRESSOR AIR FLOW, FT**3/SEC SIDE COMPRESSOR AIR FLOW, FT**3/SEC THRUST COMPRESSOR AIR FLOW, FT**3/SEC THRUST COMPRESSOR AIR FLOW, FT**3/SEC TOTAL AID FLOW, FT**3/SEC FRONT JFT AREA, FT*FT SIDE JFT AREA, FT*FT SIDE JFT AREA, FT*FT THRUST JFT AREA, FT*FT FRONT COMPRESSOR PRESSURE DIFFRENCE, LB/FT*FT FRONT COMPRESSOR PRESSURE DIFFRENCE, LB/FT*FT FRONT COMPRESSOR PRESSURE, LB/FT*FT FRONT COMPRESSOR PRESSURE, LB/FT*FT FRONT NOTZLE PRESSURE, LB/FT*FT FRONT NOTZLE PRESSURE, LB/FT*FT FRONT JFT HEAT TRANSFER, BTU SIDE JFT HEAT TRANSFER, BTU THRUST JFT HEAT TRANSFER, BTU FRONT JFT TEMPERATURE RISE, DEG, F FRAN JFT TEMPERATURE RISE, DEG, F SIDE JFT TEMPERATURE RISE, DEG, F STOR JFT TEMPERATURE RISE, DEG, F THRUST JFT TEMPERATURE RISE, DEG, F THRUST JFT TEMPERATURE RISE, DEG, F	

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